

AS Level Exam-style Practice Paper

$$1 \text{ a } a = \frac{dv}{dt} = \frac{144 - v^2}{48} \text{ ms}^{-2}$$

$$\frac{1}{144 - v^2} \frac{dv}{dt} = \frac{1}{48}$$

$$\int \frac{1}{144 - v^2} dv = \int \frac{1}{48} dt$$

Rearranging gives:

$$\frac{1}{144 - v^2} = \frac{1}{(12 + v)(12 - v)} = \frac{1}{24} \left(\frac{1}{12 + v} + \frac{1}{12 - v} \right)$$

$$\text{So } \frac{1}{24} \int \frac{1}{12 + v} + \frac{1}{12 - v} dv = \int \frac{1}{48} dt$$

$$\frac{1}{24} \ln(12 + v) - \frac{1}{24} \ln(12 - v) = \frac{t}{48} + C$$

$$\frac{1}{24} \ln \left(\frac{12 + v}{12 - v} \right) = \frac{t}{48} + C$$

$$\ln \left(\frac{12 + v}{12 - v} \right) = \frac{t}{2} + 24C$$

$$\left(\frac{12 + v}{12 - v} \right) = e^{\frac{t}{2} + 24C} = De^{\frac{t}{2}} \quad \text{where } D = e^{24C}$$

When $t = 0$ s, $v = 0 \text{ ms}^{-1}$, so $\frac{12}{12} = De^0 \Rightarrow D = 1$

$$\text{So } \left(\frac{12 + v}{12 - v} \right) = e^{\frac{t}{2}}$$

$$12 + v = 12e^{\frac{t}{2}} - ve^{\frac{t}{2}}$$

$$v(e^{\frac{t}{2}} - 1) = 12(e^{\frac{t}{2}} - 1)$$

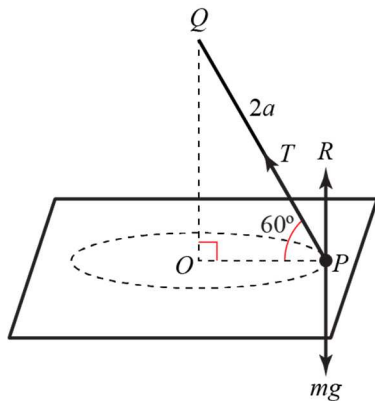
$$v = \frac{12(e^{\frac{t}{2}} - 1)}{e^{\frac{t}{2}} + 1}$$

b For all real t , $e^{\frac{t}{2}} + 1 > e^{\frac{t}{2}} - 1$

$$\text{Therefore } \frac{e^{\frac{t}{2}} - 1}{e^{\frac{t}{2}} + 1} < 1 \text{ and } \left| \frac{12(e^{\frac{t}{2}} - 1)}{e^{\frac{t}{2}} + 1} \right| < 12$$

So the speed of the particle cannot be greater than 12 ms^{-1}

- 2 a Let the tension in the string be T , the normal reaction between P and the table be R and the angular speed be $\omega = \sqrt{\frac{kg}{4a}}$



Resolving horizontally:

$$R(\leftarrow): T \cos 60^\circ = ma = m\omega^2 r \quad \text{using } F = ma \text{ and where } r \text{ is the radius of the circular motion}$$

By geometry, $r = 2a \cos 60^\circ$ so substituting for r and ω this gives:

$$T \cos 60^\circ = m \times \frac{kg}{4a} \times 2a \cos 60^\circ$$

$$T = \frac{mkg}{2} \quad \text{as required}$$

- b Resolving vertically:

$$R(\uparrow): T \sin 60^\circ + R = mg$$

$$\Rightarrow R = mg - \left(\frac{mkg}{2} \times \frac{\sqrt{3}}{2} \right) = mg \left(1 - \frac{\sqrt{3}k}{4} \right)$$

- c For the particle to remain in contact with the table, $R > 0$. Therefore

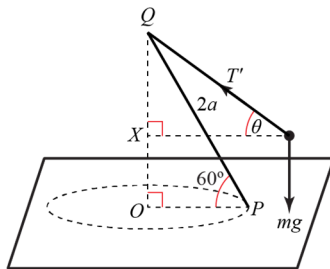
$$1 - \frac{\sqrt{3}k}{4} > 0$$

$$\frac{\sqrt{3}k}{4} < 1$$

$$\sqrt{3}k < 4$$

$$k < \frac{4}{\sqrt{3}}$$

- 2 d Let the new tension in the string be T' , the angle the string now makes with the horizontal be θ , and the angular speed be $\omega' = \sqrt{\frac{3g}{a}}$



So $QO = 2a \sin 60^\circ = \sqrt{3}a$ and $QX = 2a \sin \theta$

Resolving horizontally:

$$R(\leftarrow): T' \cos \theta = m\omega'^2 r = m \times \frac{3g}{a} \times 2a \cos \theta$$

$$\Rightarrow T' = 6mg$$

Resolving vertically:

$$T' \sin \theta = mg, \text{ so } 6mg \sin \theta = mg \text{ substituting for } T'$$

$$\Rightarrow \sin \theta = \frac{1}{6}$$

Substituting into $QX = 2a \sin \theta$ gives $QX = \frac{a}{3}$

Therefore $QX : QO = \frac{a}{3} : \sqrt{3}a = 1 : 3\sqrt{3}$ as required

- 3 a The rods are uniform, so the centre of mass of each rod is at its midpoint. The particles are treated as point masses.

Let \bar{x} be the centre of mass of the loaded framework is from AD and \bar{y} the centre of mass of the loaded framework is $3.25a$ from AB . Then using $\sum m_i r_i = r \sum m_i$, taking A as the origin, AB and AD as x - and y -axes respectively, and working round the figure in the order: AB, B, BC, C, CD, DA :

$$5m \begin{pmatrix} 2.5a \\ 0 \end{pmatrix} + 2m \begin{pmatrix} 5a \\ 0 \end{pmatrix} + 2m \begin{pmatrix} 5a \\ 0 \end{pmatrix} + 4m \begin{pmatrix} 5a \\ 2a \end{pmatrix} + 5m \begin{pmatrix} 2.5a \\ 2a \end{pmatrix} + 2m \begin{pmatrix} 0 \\ a \end{pmatrix} = (5 + 2 + 2 + 4 + 5 + 2)m \begin{pmatrix} \bar{x} \\ \bar{y} \end{pmatrix}$$

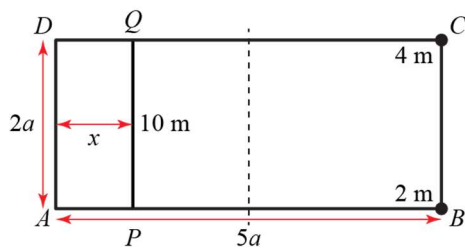
$$\begin{pmatrix} 12.5a \\ 0 \end{pmatrix} + \begin{pmatrix} 10a \\ 0 \end{pmatrix} + \begin{pmatrix} 10a \\ 2a \end{pmatrix} + \begin{pmatrix} 20a \\ 8a \end{pmatrix} + \begin{pmatrix} 12.5a \\ 10a \end{pmatrix} + \begin{pmatrix} 0 \\ 2a \end{pmatrix} = 20 \begin{pmatrix} \bar{x} \\ \bar{y} \end{pmatrix}$$

$$\begin{pmatrix} 65a \\ 22a \end{pmatrix} = 20 \begin{pmatrix} \bar{x} \\ \bar{y} \end{pmatrix}$$

So $\bar{x} = \frac{65a}{20} = 3.25a$ and $\bar{y} = \frac{65a}{20} = 1.1a$ The centre of mass of the framework lies:

- i The centre of mass of the loaded framework is $1.1a$ from AB .
- ii The centre of mass of the loaded framework is $3.25a$ from AD .

3 b Let the distance AP be x .



Treating the existing framework as a single object, taking the same axes as before and letting the centre of mass of the loaded framework including the rod PQ :

$$20m \begin{pmatrix} 3.25a \\ 1.1a \end{pmatrix} + 10m \begin{pmatrix} x \\ a \end{pmatrix} = 30m \begin{pmatrix} 2.5a \\ z \end{pmatrix}$$

$$\begin{pmatrix} 65a + 10x \\ 32a \end{pmatrix} = \begin{pmatrix} 75a \\ 30z \end{pmatrix}$$

$$10x = 75a - 65a$$

$$x = a$$

The distance AP is a

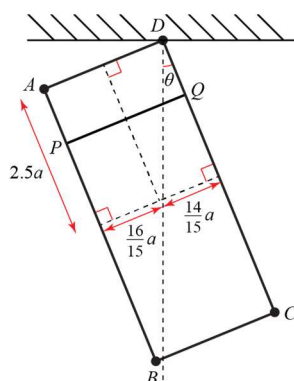
c Using part b, the distance from AB to the centre of mass also changes when PQ is added.

$$\begin{pmatrix} 65a + 10x \\ 32a \end{pmatrix} = \begin{pmatrix} 75a \\ 30z \end{pmatrix}$$

$$32a = 30z$$

$$z = \frac{32a}{30} = \frac{16a}{15}$$

The framework therefore hangs with its centre of mass directly below D and CD making an angle of θ with the vertical.



$$\text{So } \tan \theta = \frac{2 - \frac{16}{15}}{2.5} = \frac{2}{5} \times \frac{14}{15} = \frac{28}{75}$$

$$\Rightarrow \theta = 20.5^\circ \text{ (3 s.f.)}$$

The rod DC makes an angle of 20.5° (to 3 s.f.) with the vertical.

d The assumption that the rods are uniform allows the system to be modelled by assuming that the entire weight of each rod acts through its midpoint.